



## Intermodulation Measurements in Electroplated Pb-Sn Superconducting Split-loop Resonators

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Measurement of the non-linear surface impedance and intermodulation distortion (IMD) was conducted on the Linac split-loop resonators (SLR). IMD measurements allow more sensitive detection of non-linearity as compared to surface impedance measurements. All cavities were electroplated with 96%Pb4%Sn film to the final thickness of 1.5 micron followed by mechanically polishing and then re-plating with a cosmetic layer of 0.3 micron. The cavities plated with this technique display a low level of intrinsic non-linearity at operating temperature of 4.3 K and nominal absorbed RF power up to 6 W. The source of the non-linearity in the resonator structure, such as magnetic flux penetration and Josephson vortex dissipation, can be located by their contribution to the non-linear IMD response above a critical RF power level.

### 1. Introduction

The current technologies to deposit Nb film onto copper substrate are readily applied to simple RF structures but are not feasible for complex geometries like Split Loop Resonators (SLRs) and are challenging for multistub cavities, 2- and 3-QWR and 2-, 3-HWR [1]. In contrast, Pb-Sn plating provides fast and adequate results with modest equipment and at relatively low cost. ANU used Methyl Sulfonic Acid chemistry to re-plate twelve SLRs, which were electroplated earlier with fluoboric chemistry at Oxford. This change in plating chemistry increased the energy gain by almost 100%. A detailed account of the SLR plating technology at ANU is given in ref [2].

There is renewed interest in electroplated lead for use in a superconducting electron gun for the injector in free electron lasers [3]. This is because lead is a better electron emitter than niobium, the usually used material in superconducting RF devices.

### 2. Measurement surface resistance of PbSn coated SLR

The re-plating, using the hand polishing surface treatment and reverse pulse plating technique, has produced resonators with accelerating field of greater than 3.5 MV/m at 6 W during on-line test at 4.3 K. The quality factor, Q, at 6 watts is at or above  $10^8$  with the best resonator achieving  $E_{acc}$  about 3.9 MV/m on-line at 6 Watts.

The change in the surface resistance is given by equation  $R_s + jX_s = \Gamma(Q_0^{-1} - 2j(\Delta f_0/f_0))$ , where  $\Gamma = 25 \Omega$  is the SLR's geometry factor and  $\Delta f_0$  is the detuning of the cavity due to variation of surface reactance. In determination of  $\Delta f_0$ , the Lorentz force de-tuning of the SLR should be taken into account. In figure 1 the  $R_s$  at 4.3 K as a function of  $B_p$  is shown.

$R_s$  was calculated from  $Q_0$ -measurement data using the equation  $R_s = \Gamma Q_0^{-1}$ .  $R_s$  rises up to  $B_p = 4$  mT probably due to RF losses in the gasket. It remains constant from  $B_p = 4$  mT up to 35 mT followed by sharp rise due to field emission (FE).

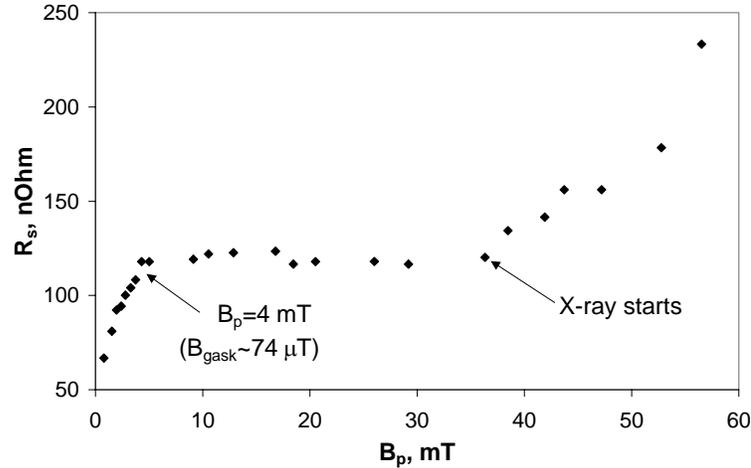


Figure 1. The surface resistance as a function of the applied microwave field at 4.3 K and 150 MHz.

### 3. Intermodulation distortion (IMD)

To investigate the power dependence of the non-linear microwave properties of the Pb-Sn plated SLR, the measurement of the two-tone intermodulation product as a function of the input power was performed in the same system configuration used for the single-tone experiment. Usually the IMD measurements are performed in a specialized resonator with a small sample inserted. In this work the IMD measurement is done on full-scale superconducting cavity with resonance frequency of 150 MHz.

In figure 2, the surface resistance  $R_s$  and the output power of the IMD third-order products as a function of the dissipated  $P_{diss}$  in the resonator power are presented at the reduced temperature  $t = T/T_c = 0.6$ .  $P_{diss}$  was calculated from the measured incident power  $P_{in}$  and the  $S$ -parameters  $S_{11}$  and  $S_{21}$ ,  $P_{diss} = P_{in}(1 - S_{11}^2 - S_{21}^2)$ .  $P_{diss}$  and  $P_{in}$  are expressed in dBm. Dissipated power  $P_{diss}$  is proportional to the square of the peak amplitude of the RF field  $B_p$ , which is the relevant intrinsic property of superconducting coating. At very small input power the IMP signals are below the spectrum analyzer noise floor and become observable when  $P_{IMD3} \geq -66$  dBm. In figure 2, the dashed line illustrates slope 3 and solid line slope 2. The arrows indicate the threshold field  $B_{ptr} \sim P_{diss}^{0.5}$  separating domains with different effects causing non-linear response in the Pb-Sn film. The  $B_{ptr1}$  and  $B_{ptr3}$  have been identified earlier from the surface resistance measurement also shown in figure 1. An operation above  $B_{ptr3} = 35$  mT gives rise of  $R_s$  due to FE.  $B_{ptr1} = 4$  mT probably indicates the threshold field where the RF losses in the gasket achieve their maximum value and then saturate. The RF gasket is in a region of low current density where the ratio  $B_{joint}/B_p$  does not exceed 2%. The maximum B-field in the RF joint at  $B_{ptr1} = 4$  mT is 80  $\mu$ T. An oxide layer of  $Pb_2O_5$  is formed on the tuner plates and gasket on exposure to air. Therefore a network of Josephson junctions or weak links may form in the vicinity of the RF joints. Due to the weak links the magnetic field penetrates much more easily than into a homogeneous superconductor. At extremely low magnetic fields, the magnetic flux may penetrate into the bulk in the form of hyper-vortices [4]. The hyper-vortices movement may be responsible for low-field microwave absorption observed in numerous experiments.

As can be seen from figure 2, the frequency transformation beyond threshold field  $B_{ptr2}$  is much more dramatic than the change in  $R_s$ . IMD represents the most sensitive characterization of the intrinsic non-linear behaviour in superconducting material. At  $B_p < B_{ptr2}$  the IMD products scale with respect to input power at 3:1. For  $B_p$  larger than  $B_{ptr2}$ , a sudden transition from slope 3 to slope 2 occurs. The behaviour above is similar in SLRs plated under identical conditions as described in [2].

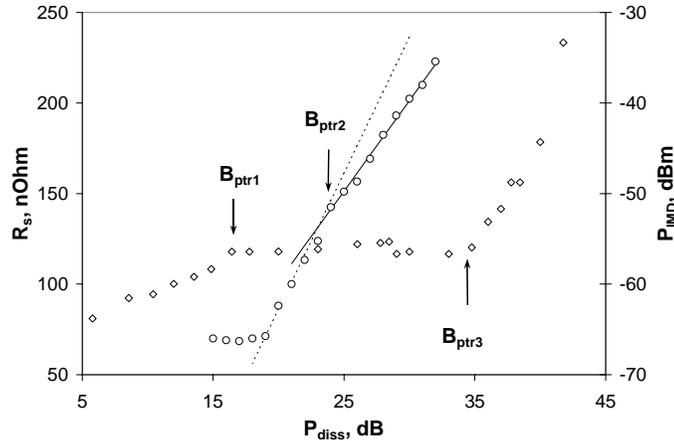


Figure 2. The surface resistance  $R_s$  ( $\otimes$ ) and the output power of the IMD products  $P_{IMD3}$  ( $\odot$ ) as a function of the dissipated power at the reduced temperature  $t=T/T_c=0.6$ . Dashed line illustrates slope 3 and solid line slope 2. The arrows indicate the threshold field  $B_p \sim P_{diss}^{0.5}$  separating domains with different nonlinear effects.

Using the harmonic balance algorithm, Mateu *et al* [5] have calculated the power dependence of the IMD products for the power-law nonlinearity in the different forms. These authors have found that the slope 2 of the third-order IMD may correspond to dissipation due to Abrikosov or Josephson vortex [5]. The estimated  $B_{ptr2} = 9$  mT is significantly lower than the  $B_{c1} = 53$  mT value estimated for 96%Pb4%Sn superconducting film. This may be explained by the fact that ANU Pb-Sn coating process involves mechanical hand polishing of the superconducting layer just before deposition of the final cosmetic layer. The mechanical polishing can damage the film and introduce voids and non-superconducting inclusions, the magnetic field can penetrate through the film at much lower field  $B_{ptr2} < B_{c1}$ .

#### 4. Conclusion

The initial rise in the surface resistance of Pb-Sn films might be caused by low-field microwave absorption due to hyper-vortices movement in the Josephson medium in the vicinity of RF joints.

In low temperature superconducting materials the third-order products must increase with the third power of input main tones. In our case, the IMD slope changes to 2 above transition magnetic field  $B_{tr2} = 9$  mT. This unconventional behaviour in our resonators upon increasing RF power might originate from a hysteresis process dominated by the creation and the irreversible motion and gradual penetration of the Josephson vortices into voids and non-superconducting inclusions introduced by mechanical polishing process.

#### Acknowledgments

We are grateful to technicians from Nuclear Physics Department J. Heighway, A. Muirhead, A. Cooper and H. Wallace for their important contribution of project.

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